

WHAT IS CLAIMED IS:

1. A position sensing apparatus for deriving rotor position of a synchronous machine from signals output from said machine, said apparatus comprising:

5 a bandpass filter that filters phase voltage signals output from main stator windings of said synchronous machine during AC excitation, thereby extracting a rotor position-indicating component from said phase voltage signals;

a converter that converts the filtered phase voltages into balanced  
10 two-phase quadrature signals, said balanced two-phase quadrature signals indicating positioning of said rotor; and

an excitation controller for controlling AC excitation frequency as a function of rotor speed, thereby increasing a position detection range of said position sensing apparatus.

15 2. The position sensing apparatus of claim 1, wherein said synchronous machine is a synchronous brushless machine.

3. The position sensing apparatus of claim 1, wherein said rotor is on a shaft coupled to a gas turbine engine of an aircraft.

4. The position sensing apparatus of claim 1, wherein said  
20 bandpass filter has a fixed passband over a range of rotor speeds.

5. The position sensing apparatus of claim 4, wherein the fixed passband is defined as a function of :

$$f_{sig} = 2 \cdot N_{ph} \cdot f_{init} + f_{e\_st} \cdot (4 \cdot N_{ph} \pm 1)$$

wherein  $f_{sig}$  is a frequency of a signal containing rotor position  
25 information,  $N_{ph}$  is a number of phases in an exciter stator,  $f_{e\_st}$  is the electrical frequency of a main stator voltage, and  $f_{init}$  is an initial AC excitation frequency.

6. The position sensing apparatus of claim 1, wherein the two-phase quadrature signals are used as inputs to emulate a position sensor in a drive system for the synchronous machine.

5 7. The position sensing apparatus of claim 6, wherein the two-phase quadrature signals are used as inputs to emulate a resolver.

8. The position sensing apparatus of claim 1, wherein a Clarke transformation is used to convert the filtered phase voltages into the balanced two-phase quadrature signals.

10 9. The position sensing apparatus of claim 1, wherein AC excitation amplitude is maintained substantially constant over a range of rotor speeds.

15 10. The position sensing apparatus of claim 1, wherein AC voltage at output terminals of the machine is maintained below a preset level due to a field weakening caused by the AC excitation frequency control.

11. The position sensing apparatus of claim 1, wherein said excitation controller varies AC excitation frequency to substantially maximize the ratio between a phase voltage frequency component carrying rotor position information and a rotor frequency component.

20 12. A position sensing method for deriving rotor position of a synchronous machine from signals output from said machine, said method comprising:

bandpass filtering phase voltage signals output from main stator windings of said synchronous machine during AC excitation, thereby  
25 extracting a rotor position-indicating component from said phase voltage signals;

converting the filtered phase voltages into balanced two-phase quadrature signals, said balanced two-phase quadrature signals indicating positioning of said rotor; and

controlling AC excitation frequency as a function of rotor speed,  
5 thereby increasing the position detection range of the position sensing method.

13. The position sensing method of claim 12, wherein said synchronous machine is a synchronous brushless machine.

14. The position sensing method of claim 12, wherein said rotor  
10 is on a shaft coupled to a gas turbine engine of an aircraft.

15. The position sensing method of claim 12, wherein said bandpass filtering is performed using a fixed passband over a range of rotor speeds.

16. The position sensing method of claim 15, wherein the fixed  
15 passband is defined as a function of :

$$f_{sig} = 2 \cdot N_{ph} \cdot f_{init} + f_{e\_st} \cdot (4 \cdot N_{ph} \pm 1)$$

wherein  $f_{sig}$  is a frequency of a signal containing rotor position information,  $N_{ph}$  is a number of phases in an exciter stator,  $f_{e\_st}$  is the electrical frequency of a main stator voltage, and  $f_{init}$  is an initial AC  
20 excitation frequency.

17. The position sensing method of claim 12, wherein the two-phase quadrature signals are used as inputs to emulate a position sensor in a drive system for the synchronous machine.

18. The position sensing method of claim 17, wherein the two-  
25 phase quadrature signals are used as inputs to emulate a resolver.

19. The position sensing method of claim 12, wherein a Clarke transformation is used to convert the filtered phase voltages into the balanced two-phase quadrature signals.

20. The position sensing method of claim 12, wherein AC  
5 excitation amplitude is maintained substantially constant over a range of rotor speeds.

21. The position sensing method of claim 12, wherein the AC  
voltage at output terminals of the machine is maintained below a preset  
limit due to a field weakening caused by the AC excitation frequency  
10 control.

22. The position sensing method of claim 12, wherein said AC  
excitation frequency control varies AC excitation frequency to  
substantially maximize the ratio between a phase voltage frequency  
component carrying rotor position information and a rotor speed  
15 frequency component.